

# Supporting Information

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## SI Text

**Cellular Elastic Model.** The total elastic energy ( $U$ ) of an *Escherichia coli* cell under a bending force can be written as:

$$U = 2U_{\text{MreB}} + U_0, \quad [\text{S1}]$$

where  $U_{\text{MreB}}$  is the elastic energy in a single MreB helical bundle, and  $U_0$  is the elastic energy in the cell wall and the other mechanical components. The coefficient 2 comes from the fact that MreB has been shown to form a double-helix in *E. coli* (1). As the stuck part of the cell does not contribute to the elastic energy, we only consider the free part of the cell in our model.

We model the cell as an elastic rod:

$$U = \frac{1}{2}A \int_0^L \kappa^2 ds, \quad [\text{S2}]$$

$$U_0 = \frac{1}{2}A_0 \int_0^L \kappa^2 ds, \quad [\text{S3}]$$

where  $A$  is the flexural rigidity of the whole cell,  $A_0$  is the flexural rigidity after A22 treatment,  $L$  is the length of the free end,  $\kappa$  is the local change in curvature of the cell during bending, and  $s$  is the arc length along the cell. We have

$$\kappa = \frac{F}{A}(L - s). \quad [\text{S4}]$$

where  $F$  is the bending force (2).

To investigate the effect of linking the MreB helix to the cell wall on bending stiffness, we considered two extreme assumptions that either the MreB bundle is tightly linked to the cell wall with infinite stiffness or that there is no linkage between the MreB bundle and the cell wall. Under the first assumption, cell bending leads to bending of the MreB bundle, the elastic energy of which is denoted as  $U_{\text{MreB,bending}}$ . In addition, the bundle on one side the cell will be locally stretched, and the bundle on the other side will be locally compressed. The elastic energy due to these conformational changes is denoted  $U_{\text{MreB,stretching}}$ . The total elastic energy of the bundle is then:

$$U_{\text{MreB}} = U_{\text{MreB,bending}} + U_{\text{MreB,stretching}}. \quad [\text{S5}]$$

The bending energy is given by

$$U_{\text{MreB,bending}} = \frac{1}{2}A_{\text{MreB}} \int_0^{L'} \kappa'^2 ds', \quad [\text{S6}]$$

where  $A_{\text{MreB}}$  is the flexural rigidity of the MreB bundle,  $L'$  is the length of the bundle,  $\kappa'$  is the local curvature change of the bundle during bending, and  $s'$  is the arc length along the helical bundle. We model the MreB bundle as a solid cylinder with radius  $a$  and Young's modulus  $E_{\text{MreB}}$ , thus

$$A_{\text{MreB}} = \frac{1}{4}\pi a^4 E_{\text{MreB}}. \quad [\text{S7}]$$

Because of MreB's helical conformation,  $L'$  is related to  $L$  by the equation:

$$\frac{L'}{L} = \frac{\sqrt{p^2 + (2\pi R)^2}}{p}, \quad [\text{S8}]$$

where  $p$  is the pitch of the MreB helix and  $R$  is the radius of the cell. Similarly,

$$\frac{s'}{s} = \frac{\sqrt{p^2 + (2\pi R)^2}}{p}. \quad [\text{S9}]$$

The coordinates of the helix before ( $\mathbf{r}_0$ ) and after ( $\mathbf{r}$ ) bending can be written as

$$\mathbf{r}_0 = \left( R \cos\left(\frac{2\pi s}{p}\right), R \sin\left(\frac{2\pi s}{p}\right), s \right), \quad [\text{S10}]$$

$$\mathbf{r} = \left( R \cos\left(\frac{2\pi s}{p}\right), R \sin\left(\frac{2\pi s}{p}\right) + \Delta y, s \right), \quad [\text{S11}]$$

where  $\Delta y$  is the displacement of the cell during bending along the cell's arc length ( $s$ ):

$$\Delta y = \frac{F}{A} \left( \frac{Ls^2}{2} - \frac{s^3}{6} \right). \quad [\text{S12}]$$

$\kappa'$  is then given by

$$\kappa' = \left\| \frac{d^2 \mathbf{r}}{ds'^2} \right\| - \left\| \frac{d^2 \mathbf{r}_0}{ds'^2} \right\|. \quad [\text{S13}]$$

We also have

$$U_{\text{MreB,stretching}} = \frac{1}{2}E_{\text{MreB}}\pi a^2 \int_0^{L'} \left( \left\| \frac{d\mathbf{r}}{ds'} \right\| - 1 \right)^2 ds'. \quad [\text{S14}]$$

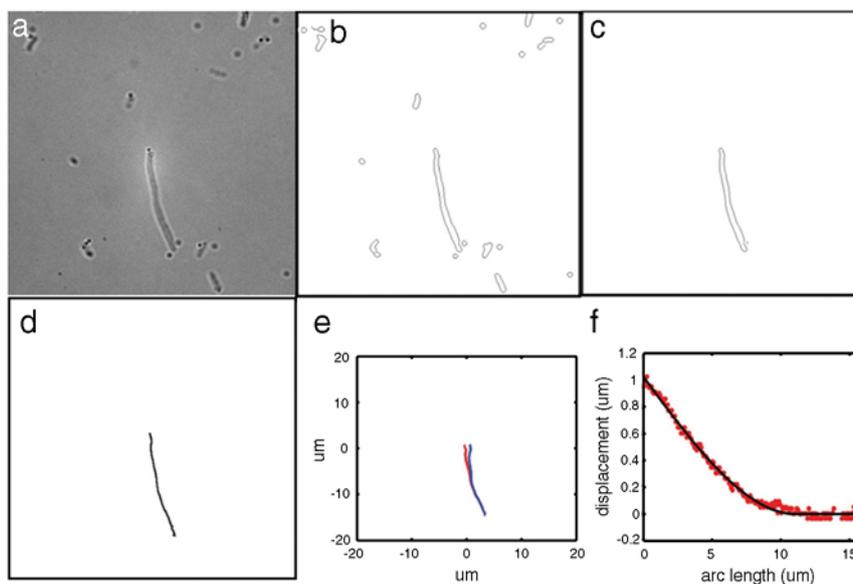
If we assume that the MreB bundle is tightly linked to the cell wall, Eqs. S5–S14 and the parameters listed in Table S2 allow us to calculate the effect of A22 on cell bending stiffness. Using several combinations of the different values of the MreB bundle pitch and protein abundance taken from the literature, we estimate that for the tightly linked bundle, the addition of A22 causes a decrease in stiffness of 96.2 to 99.7% (Table S3).

Under the second assumption, that there is no linkage between the MreB bundle and the cell wall, cell bending leads to bending but not stretching of the MreB bundle:

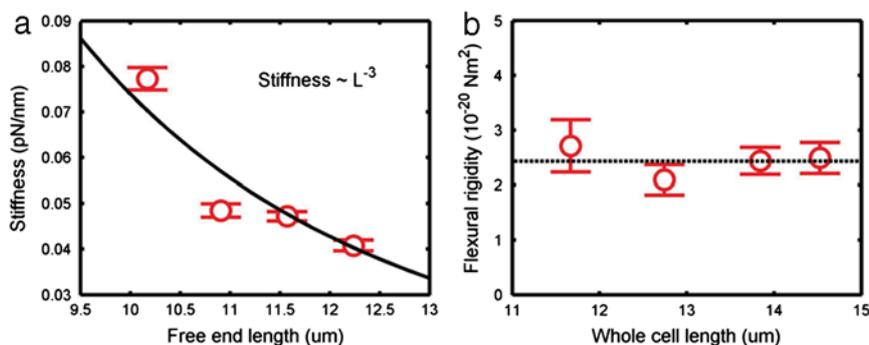
$$U_{\text{MreB}} = U_{\text{MreB,bending}}. \quad [\text{S15}]$$

If we neglect the shearing movement of the MreB helix along the arc length of the cell, the position of the helix after bending can still be expressed by Eq. S11. Using Eqs. S6–S13 and S15, and the parameters in Table S2, we predict a 0.00002% to 0.06% decrease in stiffness upon the addition of A22 (Table S3). If we had not neglected the shearing motion of the MreB helix along the cell cylinder, the helix would further relax, leading to smaller curvature change and less stored elastic energy. As a result, the true percentage would be even smaller than the calculated value above.

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**Fig. S1.** The image analysis algorithm. (A) Typical DIC image of a cell. (B) The edge of the cell was extracted by the MATLAB Canny edge detector. (C) An area of interest was manually chosen to remove the other objects in the image. (D) By averaging the edge along the major axis of the cell, we got the cell's center line. (E) The original center line of the cell (Red) and the center line of the same cell under a bending force (Blue). (F) The displacement of the center line was fit to the theoretical shape of a bent elastic rod with a stuck end.



**Fig. S2.** The stiffness and flexural rigidity of a single cell during prolonged growth. (A) The stiffness versus the free end length ( $L$ ). (B) The flexural rigidity versus the whole cell length. Strain: WX7 ( $\DeltaftsZ$ )/ $\Delta$ GL100 ( $Plac::ftsZ$ ). Error bars indicate 95% confidence intervals.





